

# Mitigation of Fatigue and Pre-Cracking Damage in Aircraft Structures Through Low Plasticity Burnishing (LPB)

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**ASIP 2007**

**Palm Springs, CA**

**December 4 – 6, 2007**



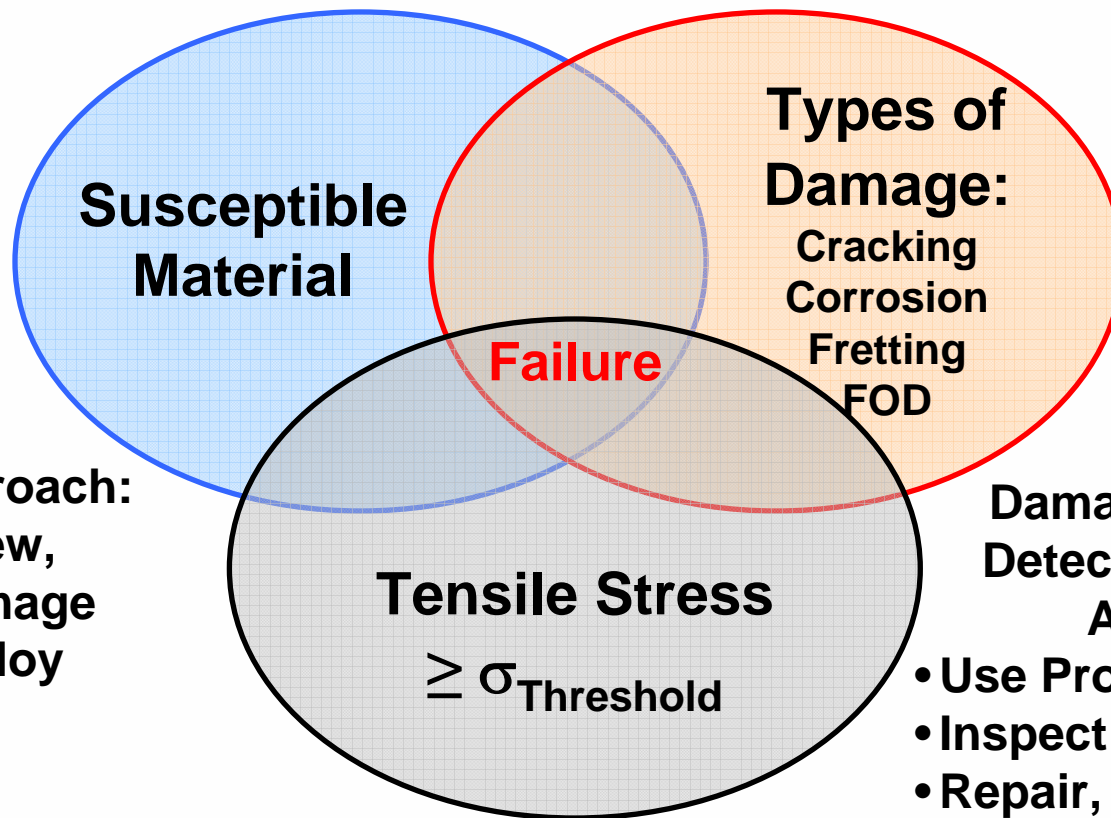
# Acknowledgement

**LPB Design, Implementation, and RS Measurement  
Conducted at Lambda Technologies**

**Part Design and Fatigue Testing Conducted at AFRL**



# Damage/Failure Susceptibility Diagram



**Materials Approach:**  
Develop new,  
tougher, damage  
resistant alloy

**Damage Prevention,  
Detection & Control  
Approach:**

- Use Protective Coatings
- Inspect for FOD, Cracks
- Repair, Blend Damage
- Replace Parts

**Residual Stress Approach:**  
“Mechanical Suppression” of Tensile  
Stresses – No need to change  
material/design & Improved damage  
tolerance



# Outline

- **Residual Stress Design Method**
- **LPB Process**
  - **Technology**
  - **Tools**
  - **Design Protocol**
  - **Production and Turnkey Installation**
- **Example of LPB to Mitigate Fatigue/Pre-Cracking Damage in AA2024-T851 Aircraft Structures**
- **Conclusions**
- **List of Current LPB Applications**



# RESIDUAL STRESS DESIGN METHOD



# Residual Stress Design Method

- **RS Design based on FDD (Fatigue Design Diagram – Lambda Patent Pending)**
- **FDD is a novel adaptation of Haigh Diagram**
- **SWT model is used to extend Haigh Diagram into compressive mean stress regime**
- **Neuber's  $k_t$  or  $k_f$  is used to account for damage**
- **Predicts  $RS_{min}$  to restore performance and  $RS_{max}$  to enhance performance**
- **RS optimization based on other design factors like part-distortion, location/magnitude of compensatory tension, etc.**

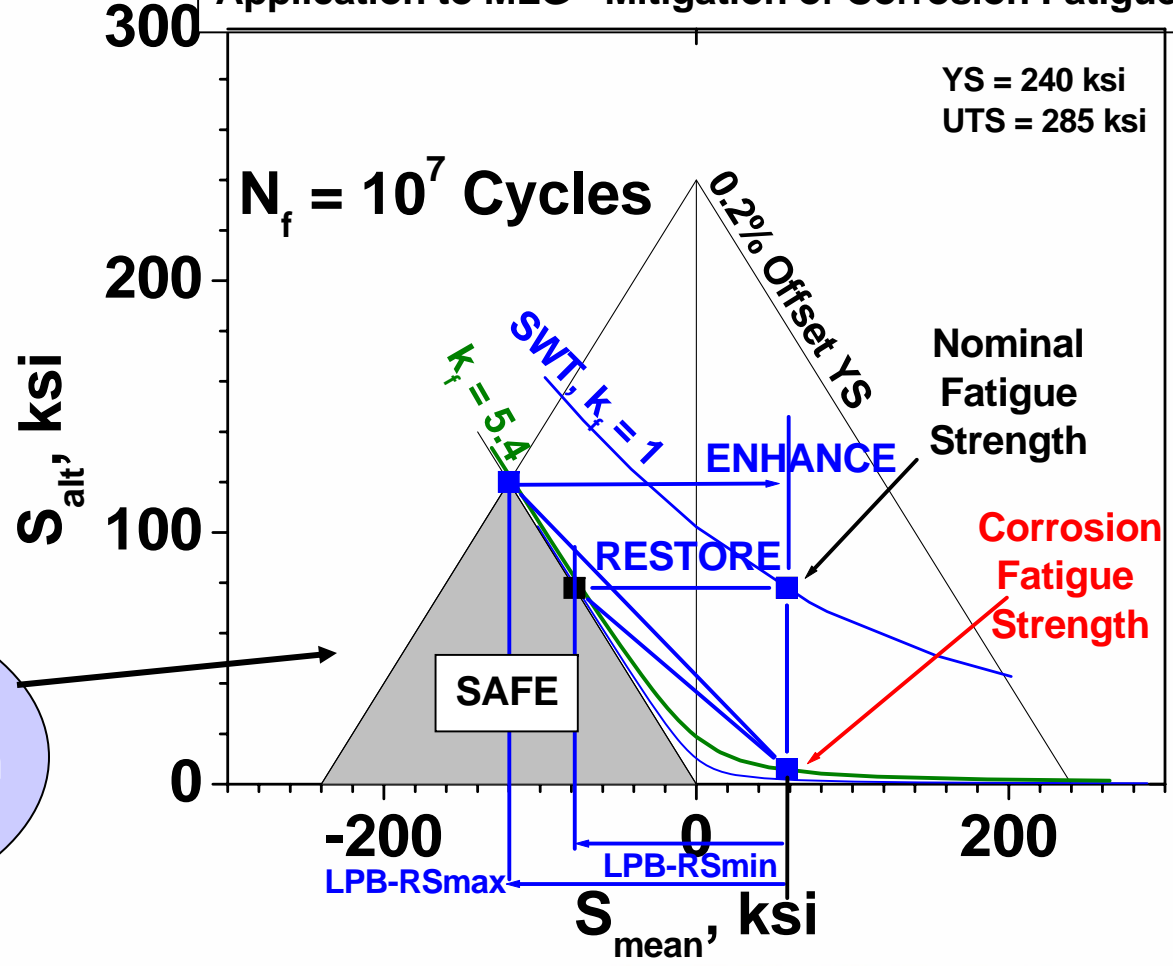


# Residual Stress Design Method

**FDD Predicts that Compressive RS Restores or Enhances Performance**

No Mode I Crack Growth in "SAFE" Region

**Fatigue Design Diagram for 300M HSLA Steel Application to MLG - Mitigation of Corrosion Fatigue**



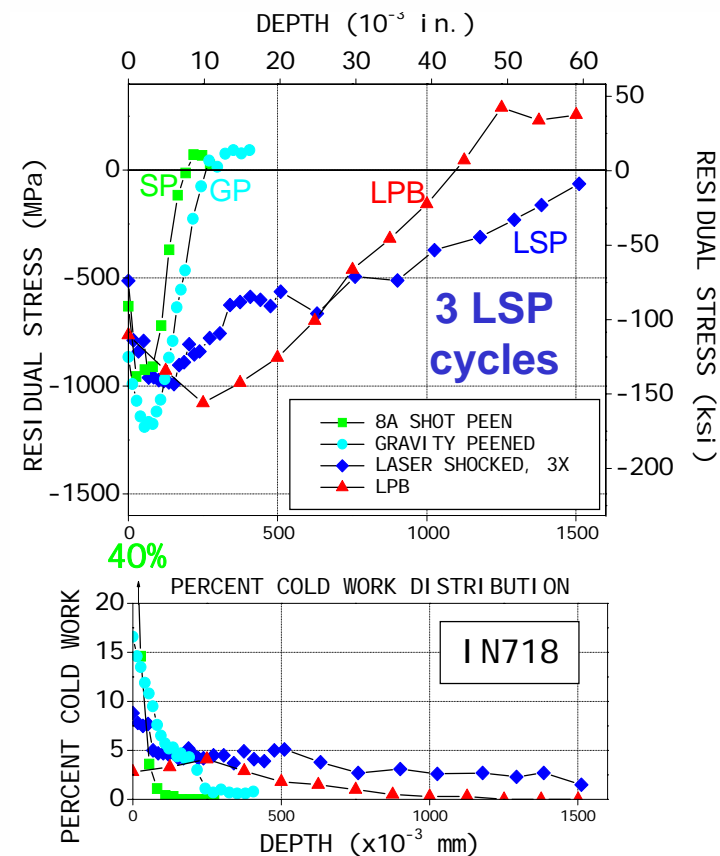
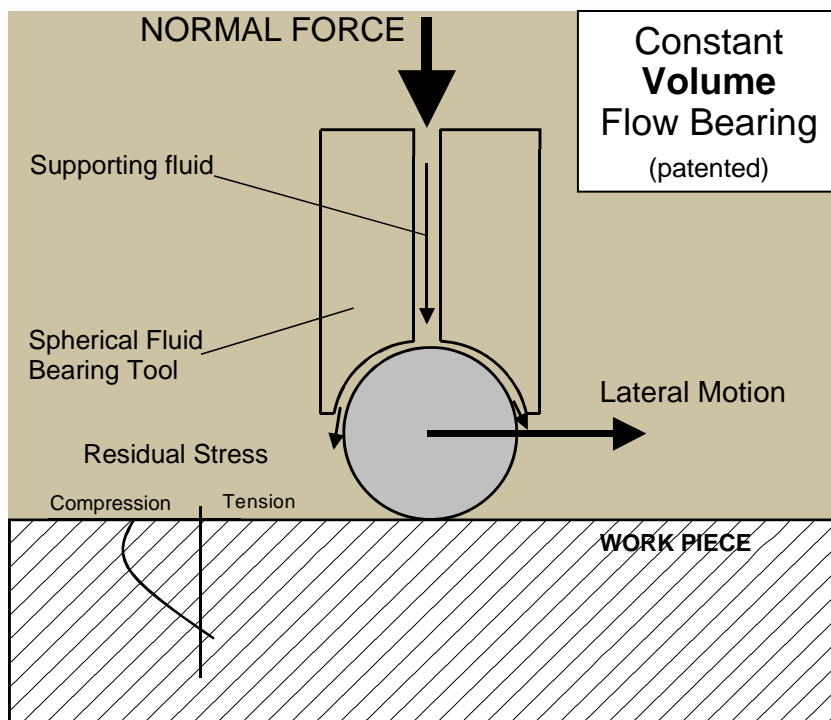
# LPB PROCESS



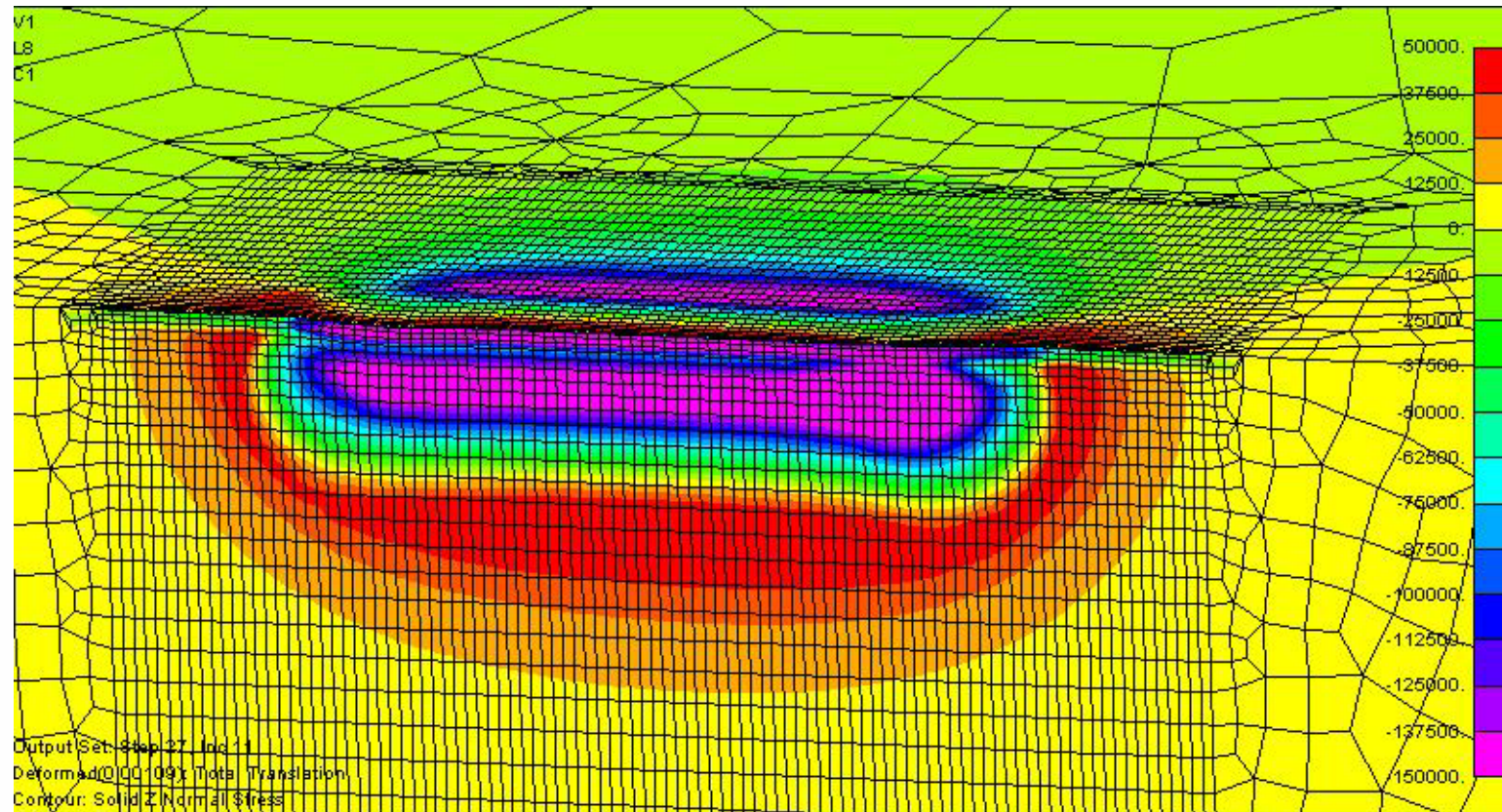


# LPB Technology

- High-hardness ball is rolled, under pressure, over surface
- Single pass provides deep compression
- Patented hydrostatic bearing with constant volume flow
- Low cold work provides stable compression

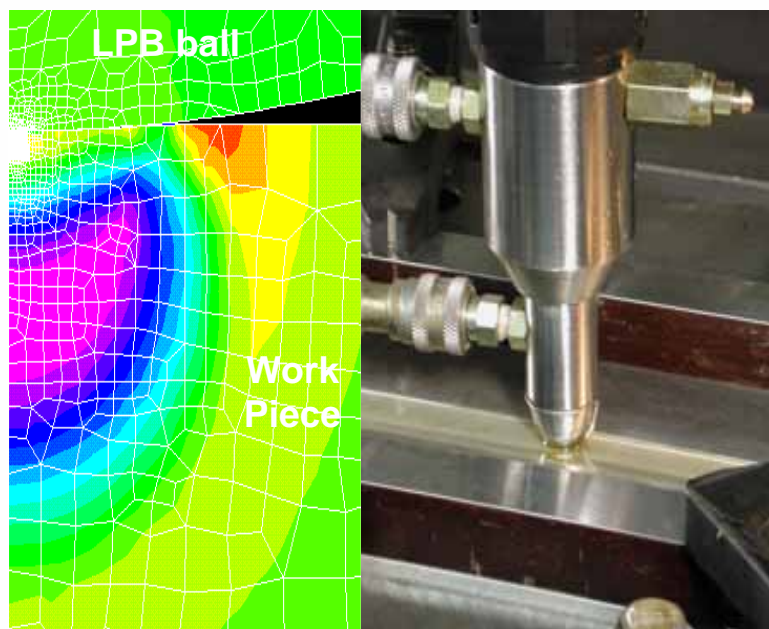


# Single Pass FEA Model of LPB Process Showing the Development of Surface and Subsurface Compression

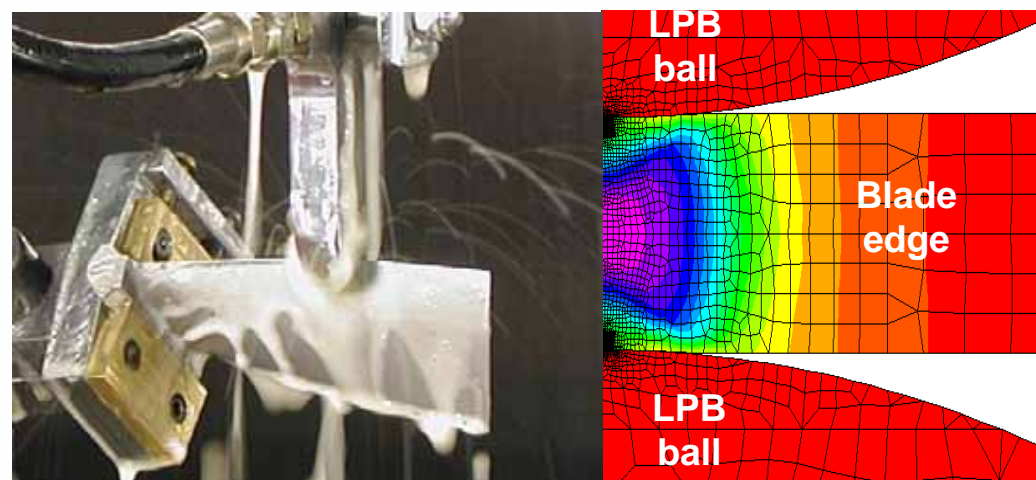


# LPB Tool Technology

**Single-Point Tool for thick pieces or one-sided application**



**Caliper Tool for thin pieces, providing through thickness compression**



Through-thickness compression in compressor blade LE

**Disk slot tools and inside calipers for ID bores built in 2006**

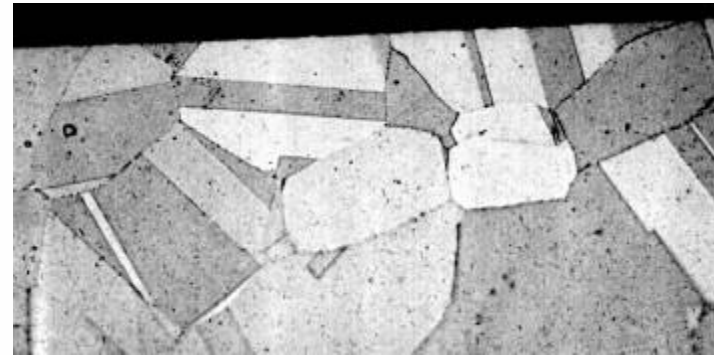




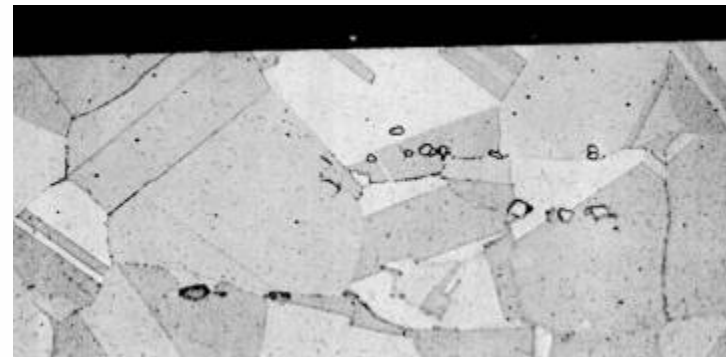
# LPB Causes No Surface Damage

- **No metallographically detectable damage at 500x**
- **Improved Surface Finish  $<10 \mu\text{in.}$**
- **Finish varies with LPB parameters: force, feed, ball type and size.**

LPB Generated Surface in IN718



Perpendicular to lay 500x



Parallel to lay 500x



# Residual Stress Stability

**Fatigue benefit is lost if residual compression relaxes.**

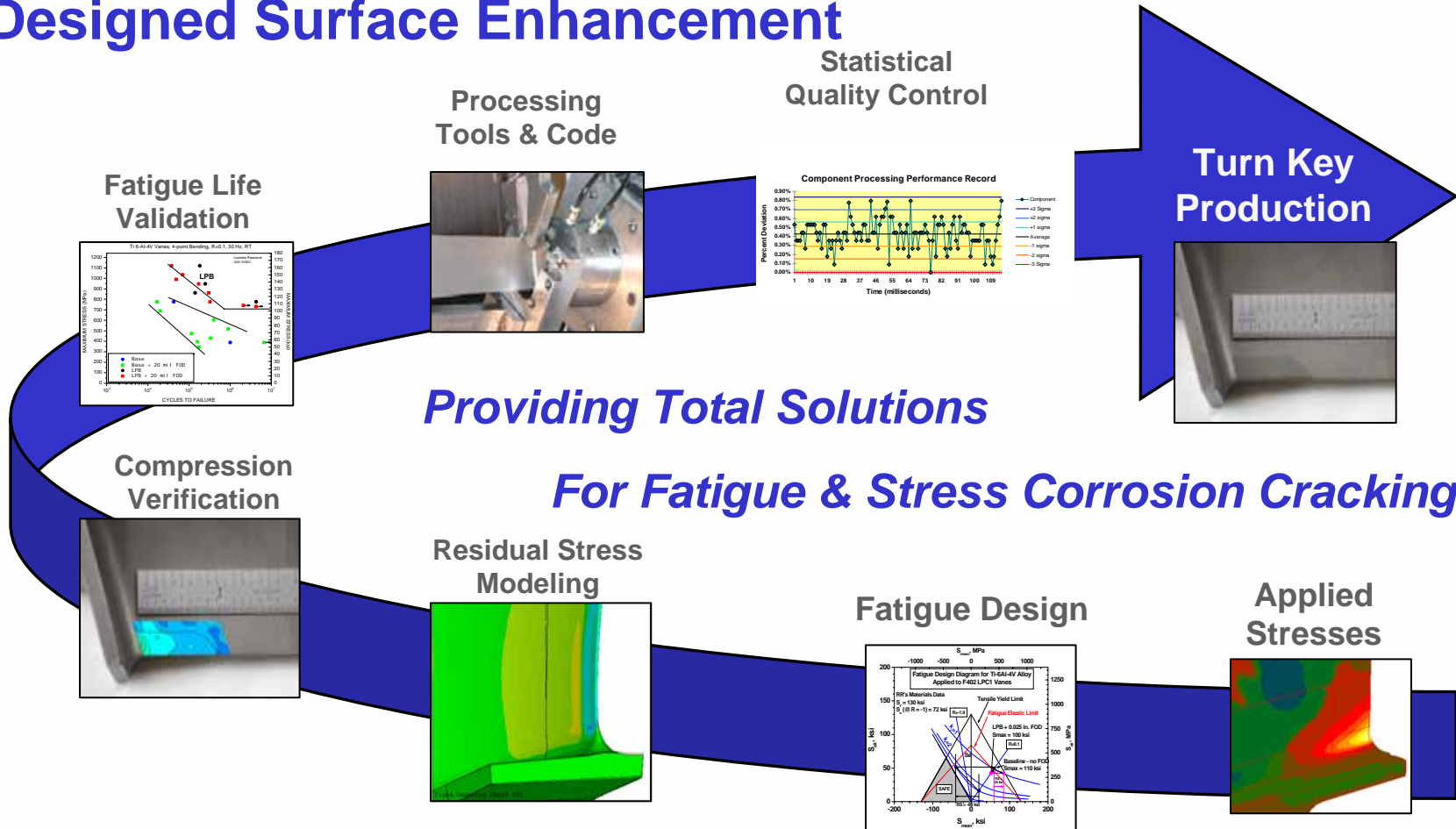
- **Thermal Relaxation**
  - Cold work increases dislocation density
  - High dislocation density increases both rate and amount of relaxation
- **Overload (Mechanical) Relaxation**
  - Cold work creates yield strength depth gradient
  - Subsequent deformation is not uniform
- **Cyclic Relaxation**
  - Not significant in HCF at  $R = S_{min}/S_{max} > 0$

**Low Cold Work = Stable Compression**



# Compressive Stress Field Design Protocol

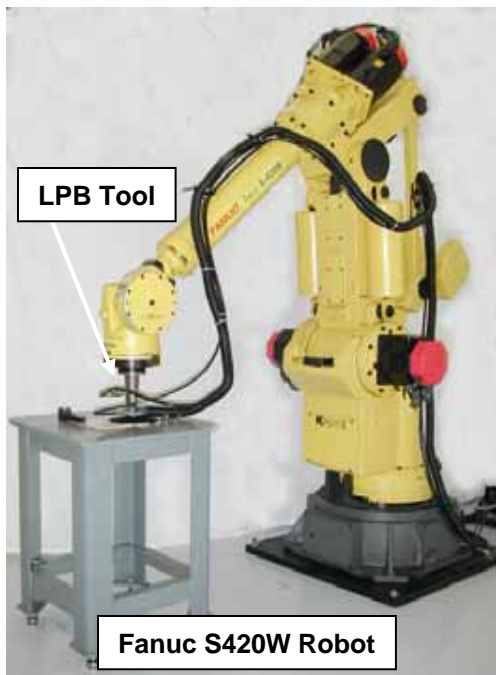
## Designed Surface Enhancement



## Total Engineering Solution: Ti-6-4 Vane



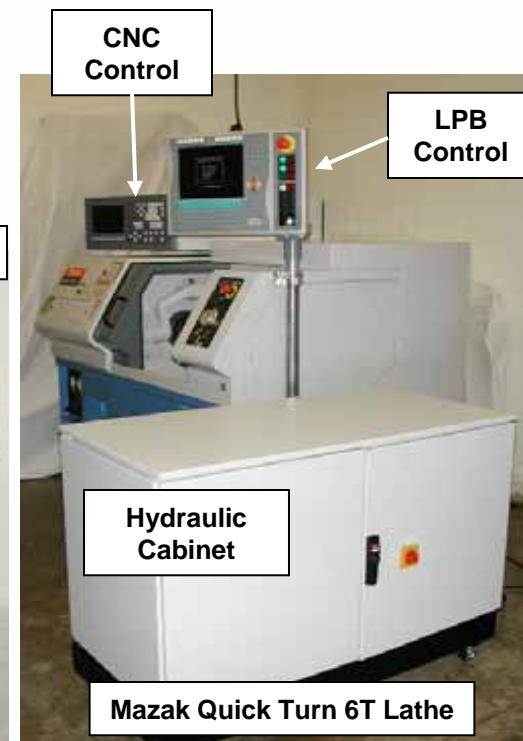
# LPB Production



**6-axis**



**4- and 5-axis**

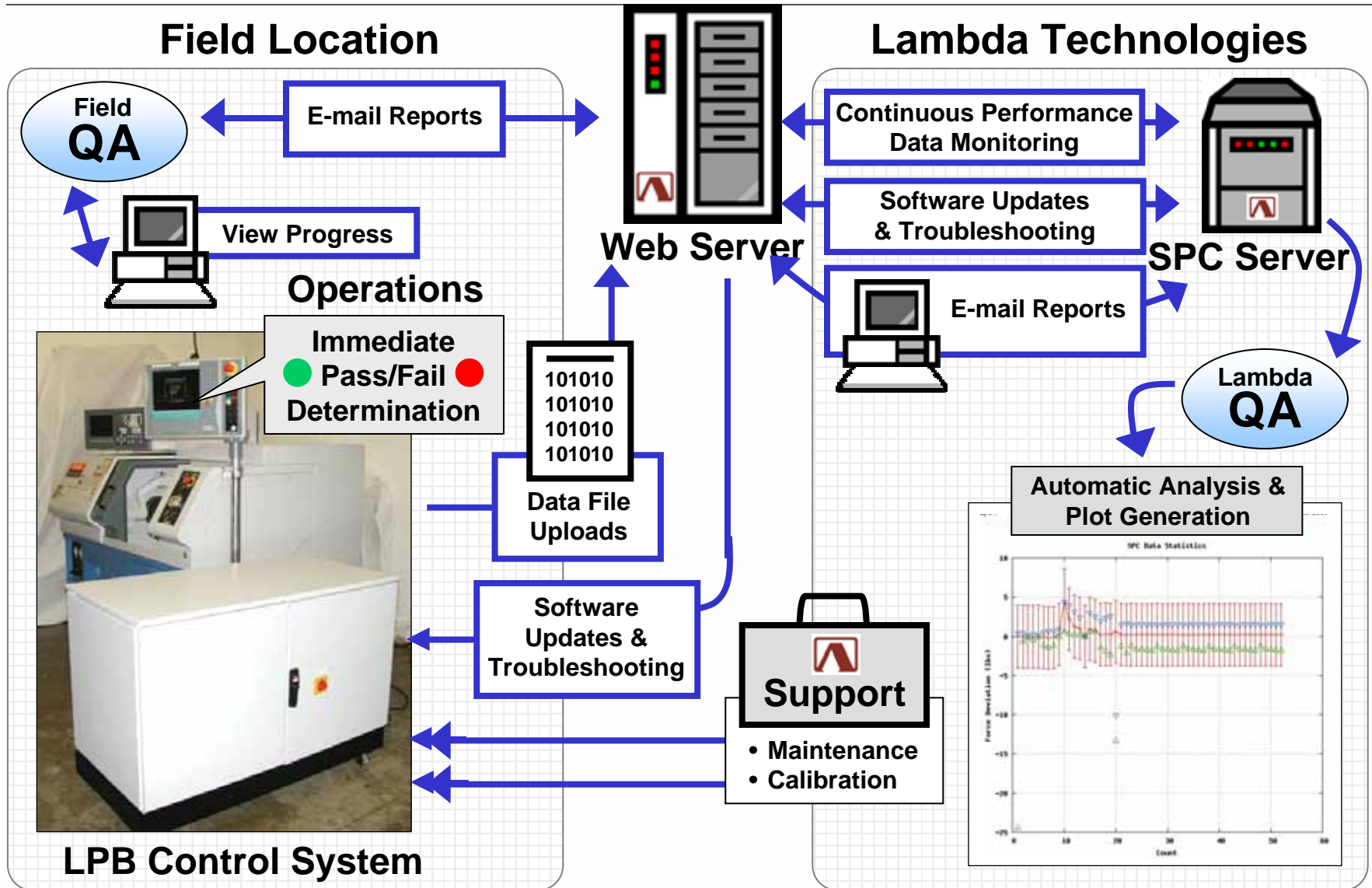


**3-axis**

- Machining-like operation using typical CNC machine tools or robots
- Highly automated...minimal operator intervention
- Low capitalization costs...use *existing* CNC machines
- Shop floor compatible...no specialized facilities



# Turn Key Field Installation





# LPB MITIGATES FATIGUE AND PRE-CRACKING DAMAGE IN AA2024-T851



# Objective of the Test Program

**To mitigate pre-cracking and fatigue damage through low plasticity burnishing (LPB) treatment in AA2024-T851 parts simulating two different features of airframe structure**



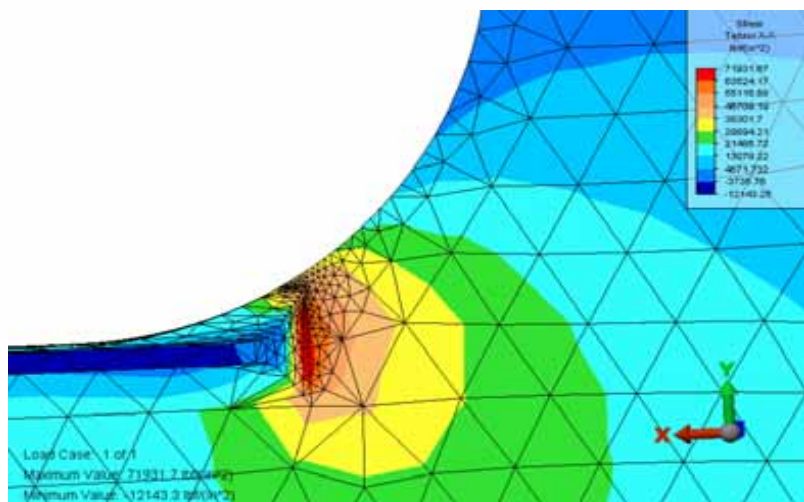
# PART DESIGN, FATIGUE TEST ARTICLES AND VARIABLES



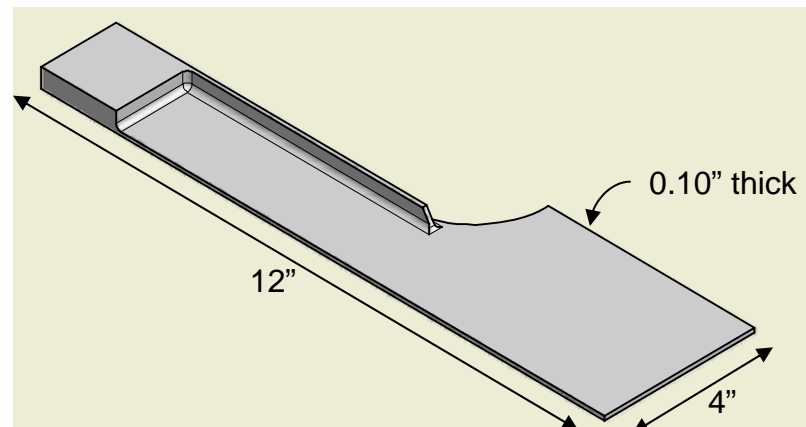
## Part A (Complex)

- Material: Al 2024 T851
- Loading (uniaxial) – Two load cases
  1. Design stress: Constant amplitude, Max stress 11.4 ksi (approximately 30,000 cycles to failure)
  2. 10% over design stress: Constant amplitude, Max stress 12.5 ksi
- R = 0.01 (ratio of min to max stress)
- Pre-crack status (0.05 in.) = yes, no
- 3-6 repetitions per test case

Part A – Applied Stress @ 4500 lb Uniaxial Load



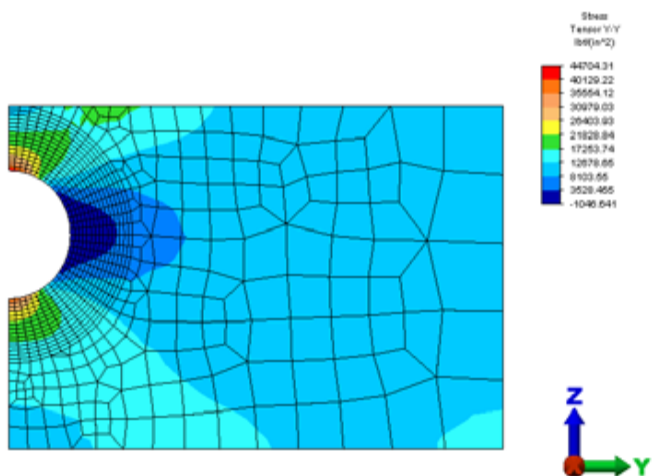
Max Stress in X-direction +72 ksi



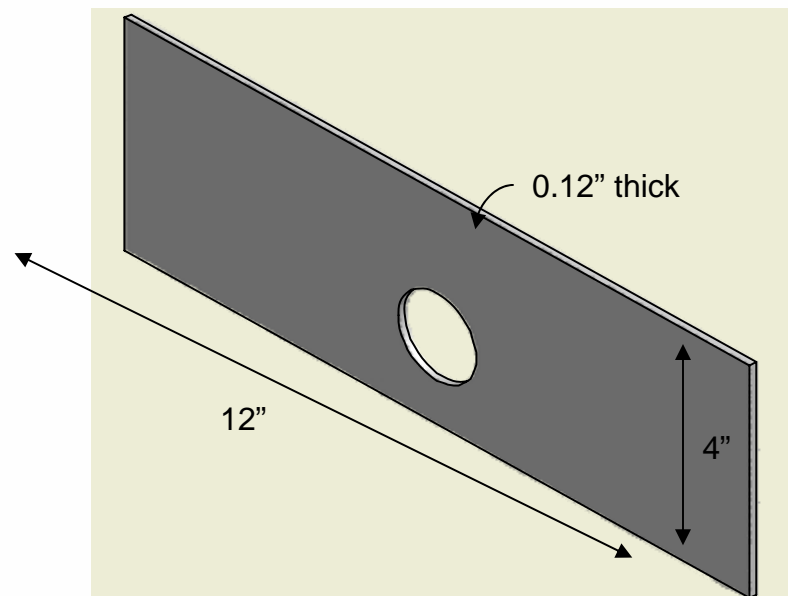
## Part B (Simple)

- Material: Al 2024 T851
- Loading (uniaxial) – Two load cases
  1. Design stress: Constant amplitude, Max stress 11.5 ksi (approximately 30,000 cycles to failure)
  2. 10% over design stress: Constant amplitude, Max stress 12.5 ksi
- $R = -1$  (ratio of min to max stress)
- Pre-crack status (0.05 in.) = yes, no
- 3-6 repetitions per test case

### AXIAL APPLIED STRESS FOR 11 KSI FAR FIELD



Load Case: 1 of 1  
Maximum Value: 44704.3 lb/(in<sup>2</sup>)  
Minimum Value: -1046.64 lb/(in<sup>2</sup>)



# RESIDUAL STRESS DESIGN, IMPLEMENTATION & MEASUREMENT



**Compressive RS is designed using Lambda's FDD (Fatigue Design Diagram) method**

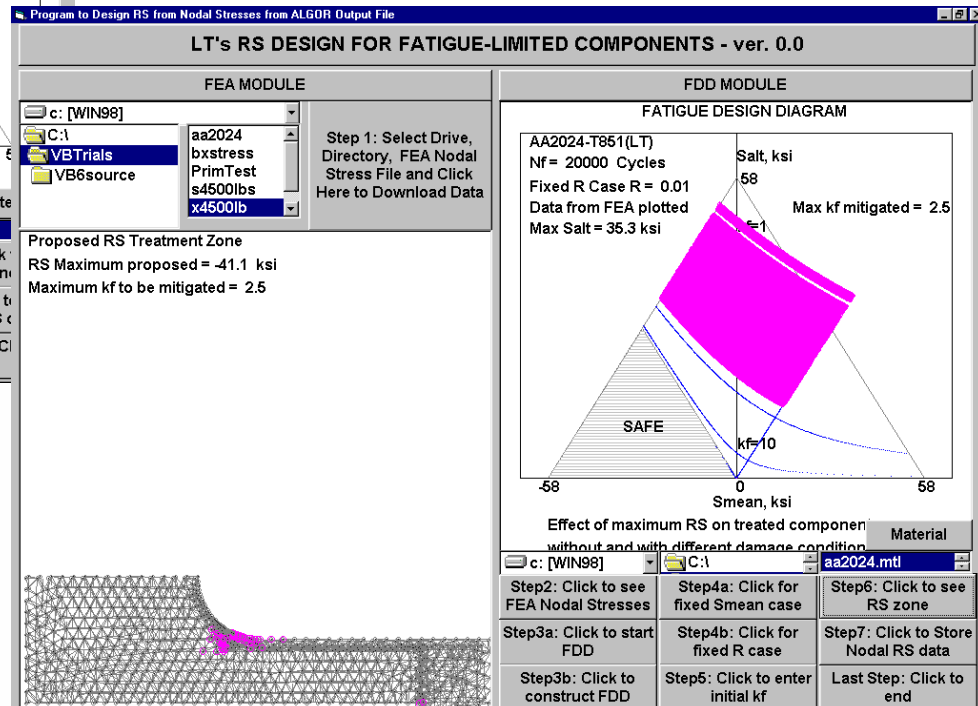
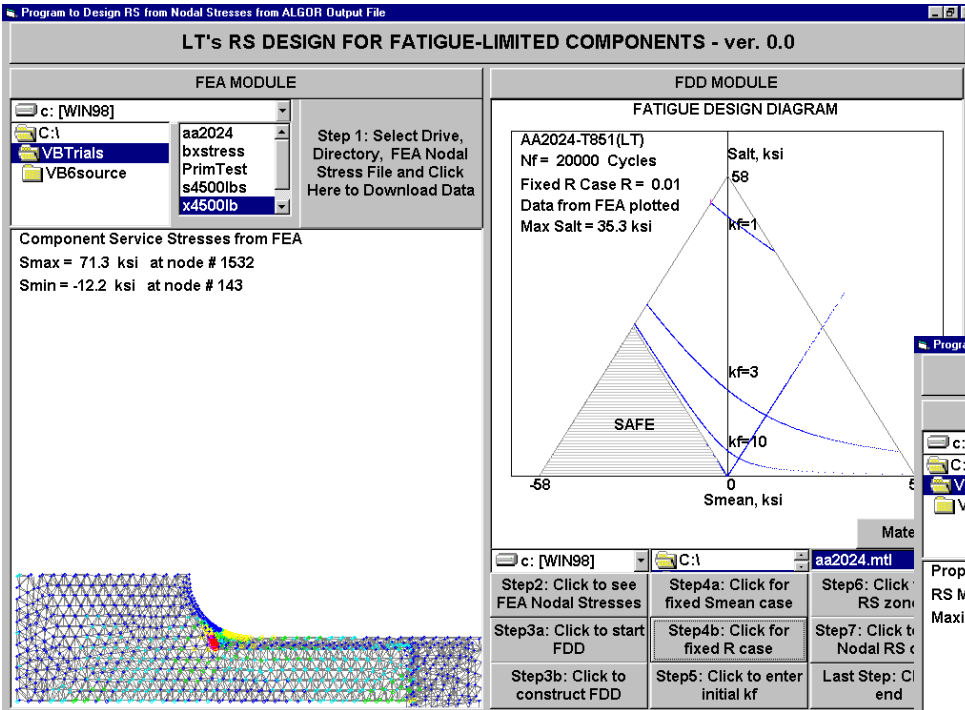
**Both controlled magnitude and depth of compression introduced at critical locations through LPB treatment**

**RS measured by x-ray diffraction method**



# LPB DESIGN – FDD METHOD

Compressive RS magnitude & locations to mitigate damage are determined by FDD (Fatigue Design Diagram)



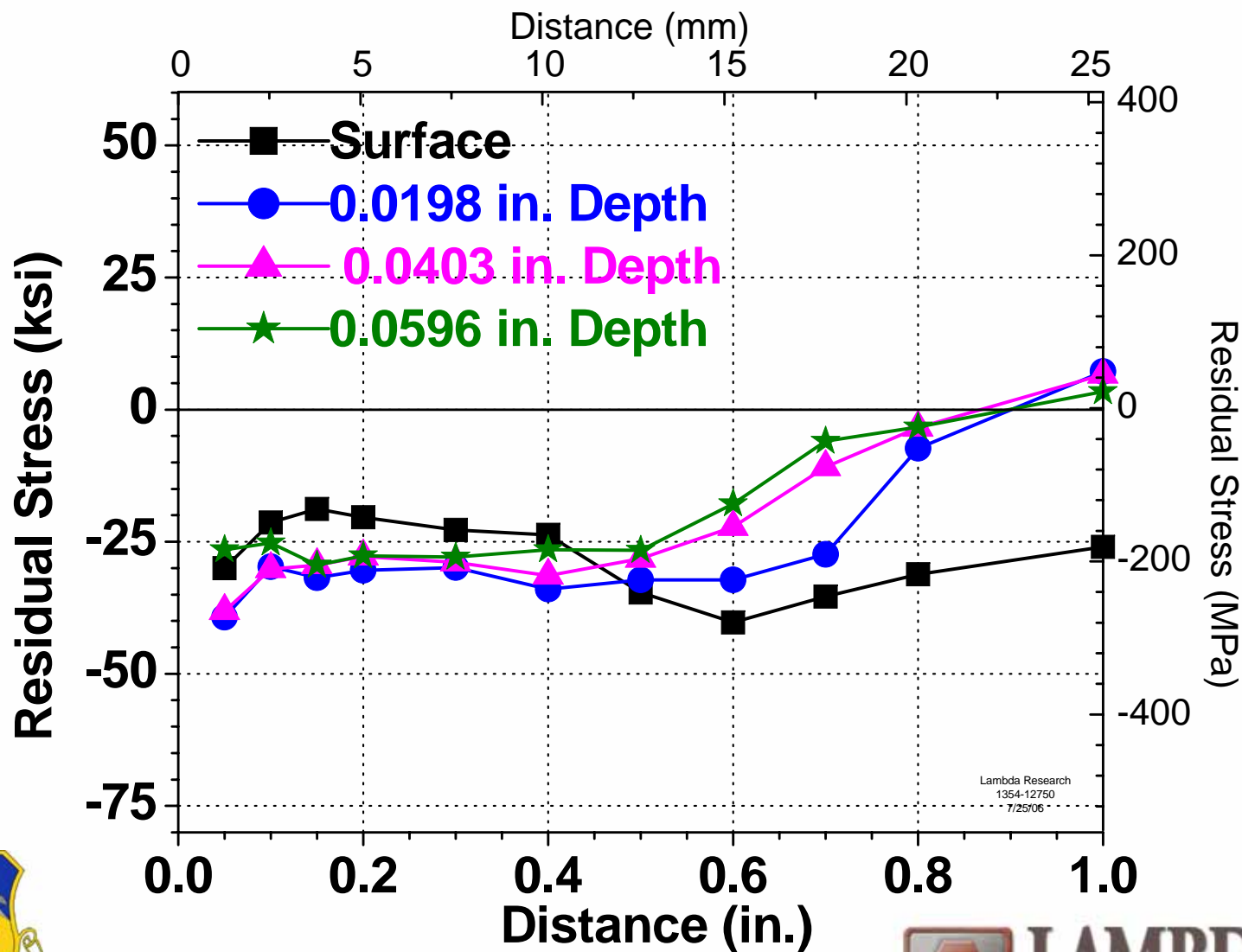


# RESIDUAL STRESS MEASUREMENTS



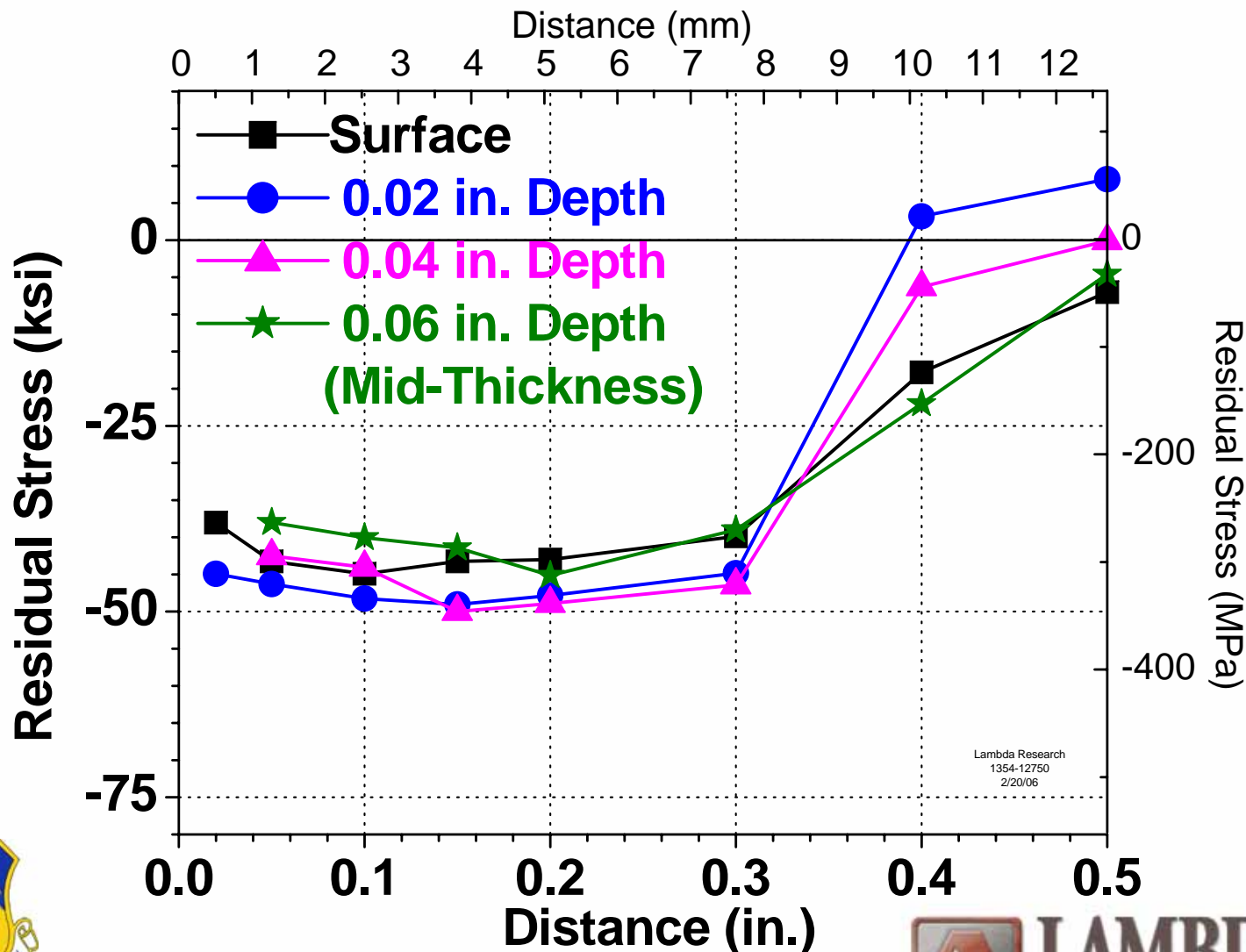
# Residual Stresses – Part A (Complex)

## TANGENTIAL RESIDUAL STRESS DISTRIBUTION



# Residual Stresses – Part B (Simple)

## LONGITUDINAL RESIDUAL STRESS DISTRIBUTION

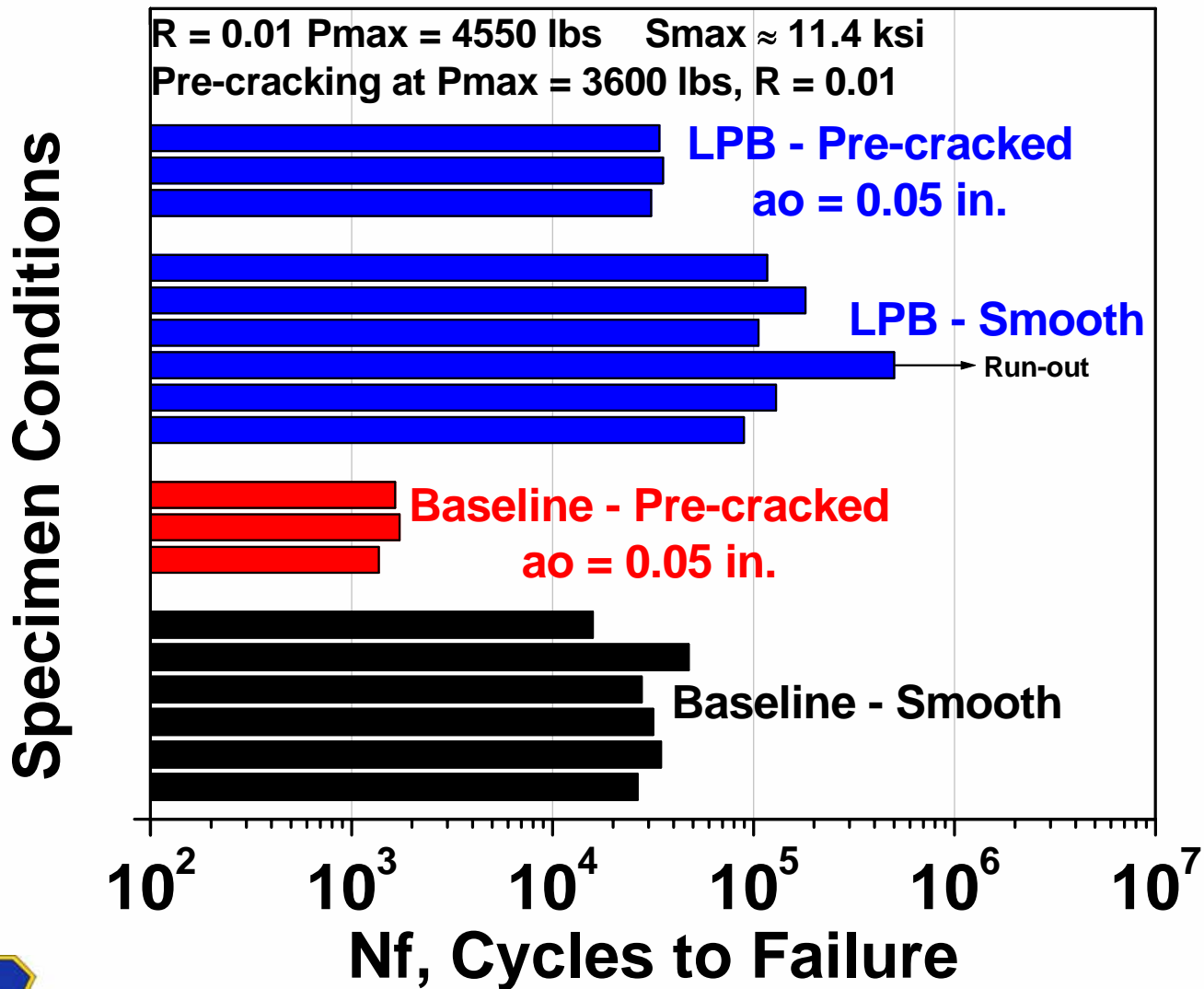


## Summary of Fatigue Test Results

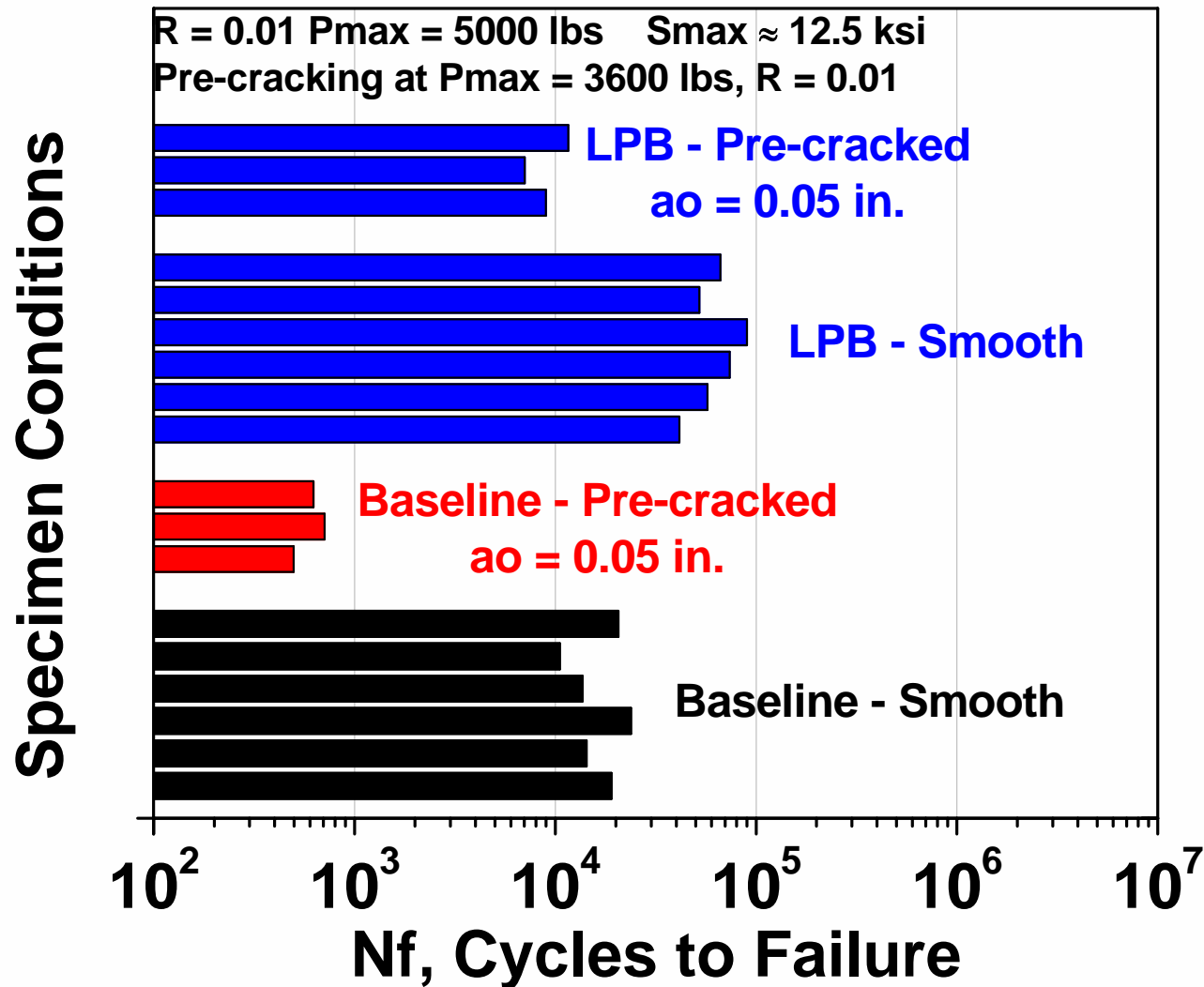
- **Fatigue life of the smooth undamaged part was decreased by a factor of 20 due to 0.050 in. precracking damage**
- **LPB improved fatigue life of smooth undamaged part by nearly a factor of 5**
- **LPB completely mitigated the precracking damage by restoring fatigue performance to that of a smooth undamaged part**



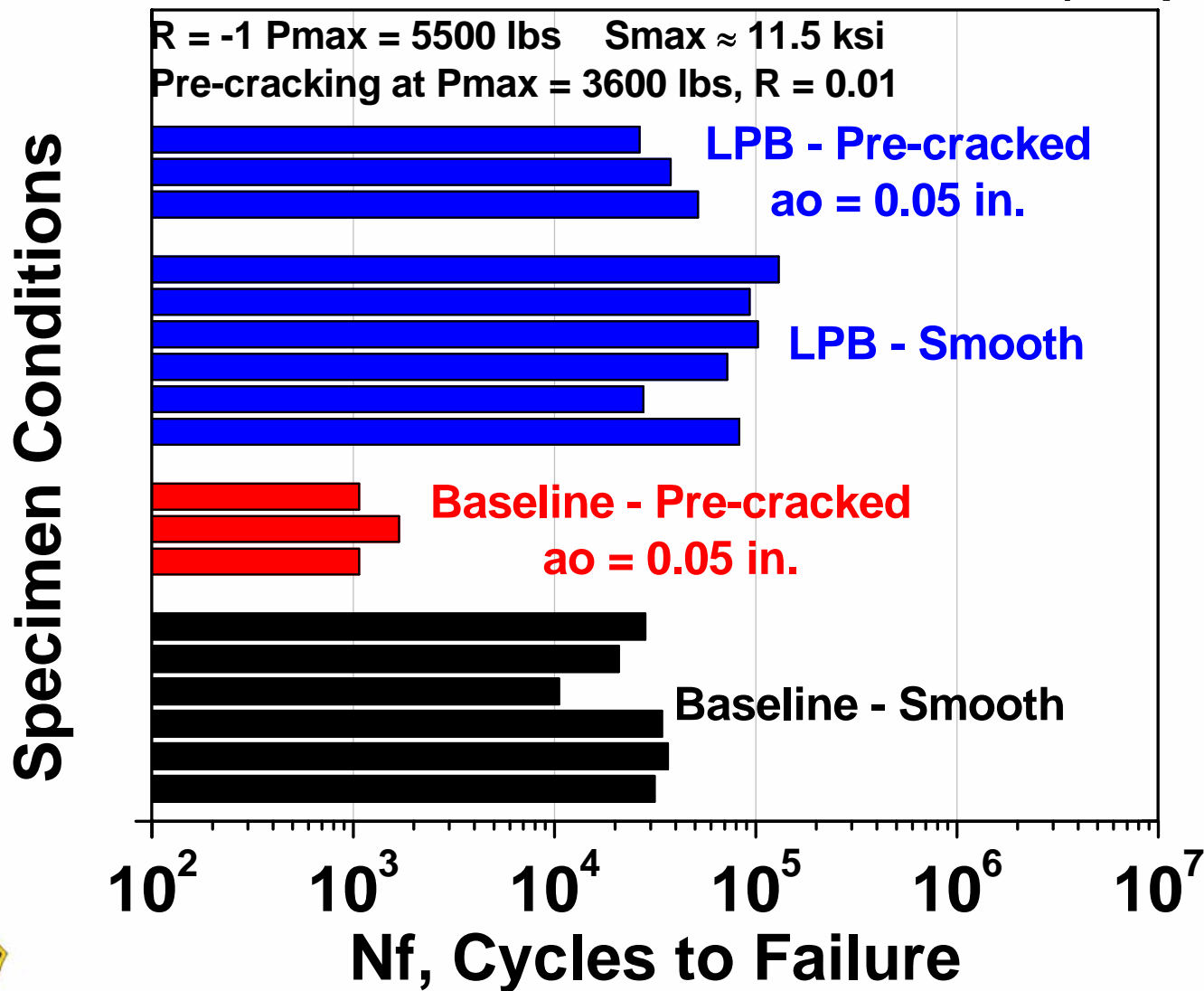
## AA2024-T851 Structural Test Panel - Part A (Complex)



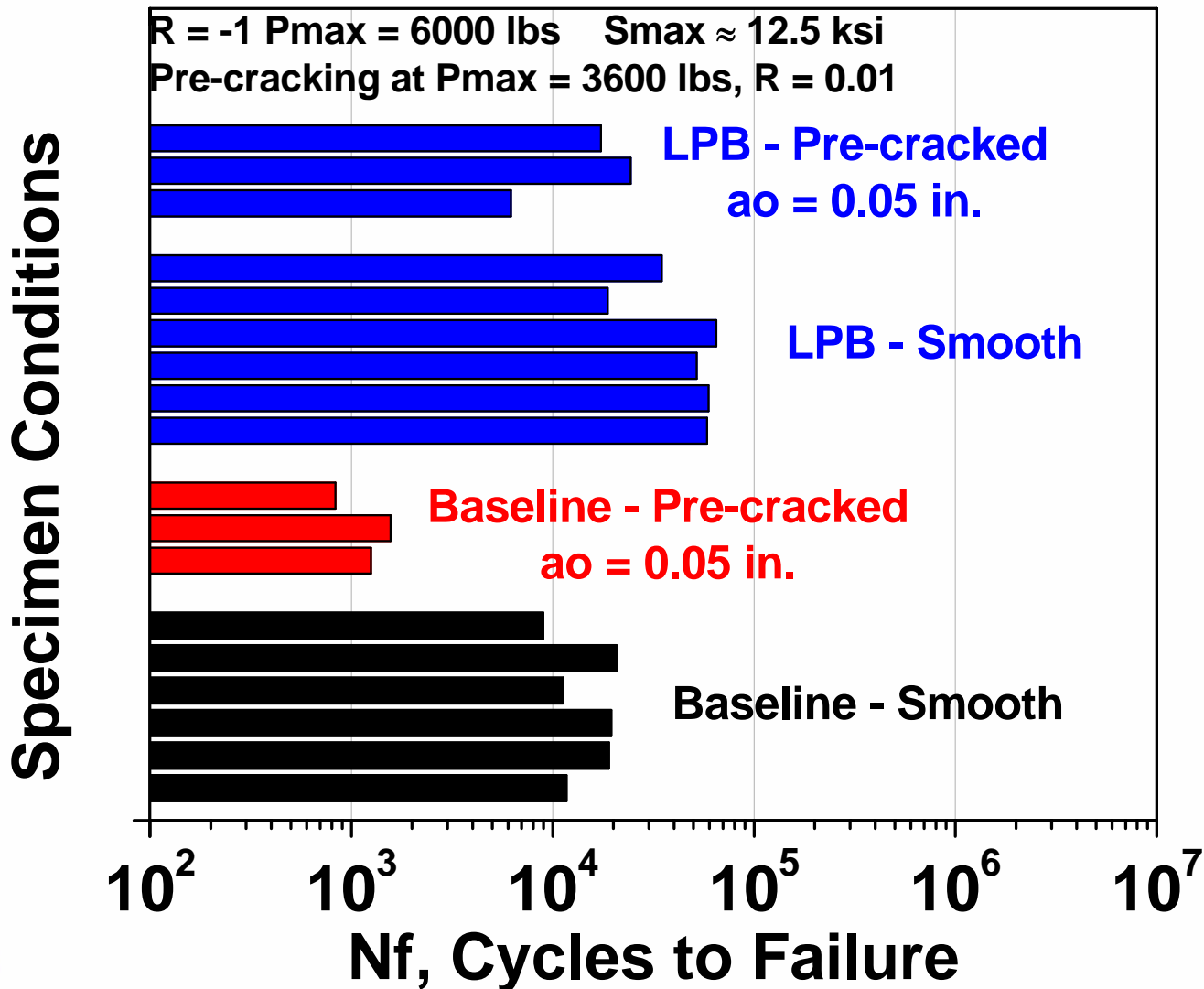
## AA2024-T851 Structural Test Panel - Part A (Complex)



## AA2024-T851 Structural Test Panel - Part B (Simple)



## AA2024-T851 Structural Test Panel - Part B (Simple)





# Summary

- **The magnitudes and locations of needed compressive RS were determined by the FDD (Fatigue Design Diagram) Method**
- **LPB treatment was designed to introduce the intended compressive RS into the locations chosen for Parts A and B**
- **RS distribution in the treated parts was verified by x-ray diffraction method**
  - **In Part A (Complex) nominally uniform compressive RS of  $-30$  ksi was achieved up to mid-thickness at critical locations**
  - **In Part B (Simple) nominally uniform compressive RS of  $-45$  ksi was achieved up to mid-thickness at critical locations**



## Summary (cont'd)

- **Fatigue test results validated predictions**
  - **LPB almost doubled the fatigue life of both smooth parts A & B**
  - **In both Parts A & B, pre-cracks (0.05 in. long) reduced the fatigue life by nearly an order of magnitude**
  - **In both Parts A & B, LPB fully restored the fatigue life of the pre-cracked (of length 0.05 in.) parts to that of smooth baseline parts**
  - **The benefits of LPB were consistently evident at both stress levels of 11.5 and 12.5 ksi**
  - **The benefits of LPB were consistently evident at both stress ratios (R) of 0.01 and -1**

